Paper-Based Laser-Pyrolyzed Electrofluidics: An Electrochemical Platform for Capillary-Driven Diagnostic Bioassays

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Microfluidic paper-based analytical devices (μPADs) are indispensable tools for disease diagnostics. The integration of electronic components into μPADs enables new device functionalities and facilitates the development of complex quantitative assays. Unfortunately, current electrode fabrication methods often hinder capillary flow, considerably restricting μPAD design architectures. Here, laser-induced graphenization is presented as an approach to fabricate porous electrodes embedded into cellulose paper. The resulting electrodes not only have high conductivity and electrochemical activity, but also retain wetting properties for capillary transport. Paper-based electrofluidics, including a lateral flow device for injection analysis of alkaline phosphatase in serum and a vertical flow device for quantitative detection of HPV16 with a CRISPR-based assay are demonstrated. It is expected that this platform will streamline the development of diagnostic devices that combine the operational simplicity of colorimetric lateral flow tests with the added benefits and possibilities offered by electronic signaling.

1. Introduction

Microfluidic paper-based analytical devices (μPADs) are an important class of microfluidic devices capable of performing total (bio)chemical analysis at ultralow cost.[1] The strength of μPADs lies in their ability to move fluids via passive capillary action without the need for external fluid actuation, thus enabling complex bioassays with extraordinary simplicity.[2]

integration of electronic components into μPADs has attracted substantial attention for its potential to realize new functionalities and capabilities. Indeed, the incorporation of electrodes opens the door to quantitative electrochemical detection,[3] assay miniaturization[4] and advanced connectivity (e.g., via near-field wireless communications).[5,6] However, electrode fabrication on paper is immensely challenging due to the rough and inhomogeneous nature of cellulose materials. In addition, the cost and complexity of current fabrication techniques hinder single-use applications.

Dungchai et al.[7] reported electrochemical detection on paper using screen-printed electrodes. Since then, a wide variety of deposition techniques have been developed and further refined, including inkjet printing,[8,9] screen printing,[10–12] metal sputtering,[13] and pencil drawing.[16] Most of these techniques are derived from conventional manufacturing processes for printed electronics. However, these deposited electrodes are often hydrophobic, hinder capillary flow and display limited contact with the fluid within pores.

There have been several attempts to circumvent these limitations. For example, Hamedi et al.[17] reported paper-based devices incorporating embedded electrodes and microfluidics through the combination of wax channel patterning and drop-cast conductive inks. They showcased a variety of electronic circuits triggered by capillary flow. Nevertheless, these approaches do not allow independent patterning of flow paths and electronic circuit traces. This means that the electrodes are constrained within the channel boundaries and it is not possible to fabricate multiple electrodes separated with electrolytes on a single sheet. This considerably limits potential applications within electrochemical sensing.

Very recently, researchers have begun to explore the direct conversion of insulating polymers, such as polyimide (Kapton)[18] and a variety of commercial polymers,[19] to conductive graphenic materials using CO2 laser cutters/engravers. In particular, laser-pyrolyzed polyimide substrates have been used in a number of biosensing applications, including small molecule detection,[20–22] protein-based immunoassays,[23,24] and DNA[25]
or miRNA\textsuperscript{[24]} recognition. Laser-induced pyrolysis of cellulose is a comparatively nascent field and to date has been exploited for artistic depictions,\textsuperscript{[26]} simple electric circuits,\textsuperscript{[27]} mechanical sensing,\textsuperscript{[28,29]} and more recently small molecule detection.\textsuperscript{[30–33]} Despite early successes, it remains unclear whether cellulose has any advantage over polyimide as a substrate material for laser-induced graphenic electrodes (LIG-Es), aside from biodegradability.

Inspired by recent progress in laser-induced graphenization, we present a method for patterning electrofluidic paths directly onto cellulose. We show that these patterns can be used to transmit both fluid and electrical currents and can be leveraged to create novel electrochemical biosensing assays. Ultimately, this work demonstrates that cellulose paper is an ideal substrate for LIG-Es, and paves the way toward a range of novel sensing applications.

2. Results

The electrochemical paper platform presented here relies on the combination of wicking channels and electronic signal traces. The intertwined patterns of these two components are embedded in a sheet of cellulose paper and together create functional electrofluidic layers. The fabrication process is as follows (Figure 1a).

First, paper-embedded electrodes are generated via laser-induced pyrolysis, harnessing the high carbon content of cellulose to create graphenic conductive traces in situ. Next, fluidic channels are formed by laminating wax onto the cellulose. It is noteworthy that the patterns for electrodes and channels are fully independent, enabling the fabrication of individually isolated and superimposed regions, with full control over wetting and conductive properties (Figure 1b). Remarkably, the process is scalable; per A4 sheet of cellulose paper, we can fabricate up to 176 sets of electrodes within 90 min at a cost of under $0.02 per sensor at a prototyping scale (Figure 1b and Table S1, Supporting Information).

2.1. Understanding the Formation of Laser-Induced Graphenic Paper

We first set out to elucidate the mechanisms underpinning the laser-induced pyrolysis of cellulose. Despite the rapidly growing interest in laser-induced graphenization, underlying mechanisms remain poorly understood.\textsuperscript{[34]} The pyrolysis of polyimide involves the transformation of a homogeneous polymer solid into a foam-like structure due to the rapid generation of gaseous products during the photothermal process.\textsuperscript{[18,35]} Controlled pyrolysis of cellulose had been shown to be challenging, due to the porous and fragile nature of the substrate, as well as its high oxygen content and lack of aromaticity. After extensive experimentation, we were not able to find a suitable process window for successful graphenization while preserving its structural integrity. To overcome this obstacle, two key parameters are indispensable: pretreatment with a fire-retardant solution and laser defocusing.\textsuperscript{[19,26]} The former prevents complete combustion of the cellulose fibers by promoting recombination reactions, and the later effectively exposes the substrate to multiple laser pulses. To explore this idea, we screened a number of inorganic fire-retardant salts together with different laser parameters. We identified ammonium sulfamate as the best pretreatment agent, yielding a sheet resistance as low as 23 ± 2 Ω sq\textsuperscript{−1} (Figures S1 and S2, Supporting Information). It should be noted that this value is significantly lower than previously reported sheet resistances\textsuperscript{[12,13]} and comparable to laser-pyrolyzed polyimide (down to 15 Ω sq\textsuperscript{−1}, Table S2, Supporting Information).\textsuperscript{[18]} The pretreatment salt is effectively rinsed off after lasing.

Next, taking inspiration from furnace-based pyrolysis,\textsuperscript{[35–37]} we employed Raman spectroscopy and wide-angle X-ray scattering (WAXS) to investigate the formation of graphenized cellulose (Figure 2). We examined laser powers between 1.2 and 4.8 W at 10 mm laser defocus and a speed of 16 cm s\textsuperscript{−1}. The lower bound approximately corresponds to the power that results in a degree of visible carbonization, and the upper bound corresponds to the maximum power the paper can endure without compromising mechanical integrity (Figure 2a and Figure S2, Supporting Information). At low powers, we observed superficial carbonization of cellulose fibers with no detectable conductivity (Figure 2b), while increasing the power beyond 2.4 W led to a sudden drop in sheet resistance.
Figure 2. Unveiling the formation and structure of laser-pyrolyzed cellulose paper. a,b) Photographs of LIG-Es fabricated using variable laser powers (a) with corresponding sheet resistances (b). c) Confocal Raman spectra for the considered samples, showing the emergence of the D, G, and 2D bands that are characteristic of graphenic materials \( n = 3–4 \). d) WAXS diffractograms for the pyrolyzed materials, with the (002), (10) and (11) diffraction peaks highlighted. Inset: schematic of a nanographitic crystallites with lateral size, \( L_a \), thickness, \( L_c \) and interlayer spacing, \( d_{002} \). e) Comparison of spectroscopic parameters extracted from Raman and XRD measurements as a function of laser power. f) Cross-sectional SEM images for a cellulose fiber before (top; orange) and after (bottom; purple) laser-induced pyrolysis. Scale bars: 5 \( \mu \)m. g) Top-view SEM image of a cellulose-LIG-E interface revealing the morphological transition. Scale bar: 100 \( \mu \)m. h) Corresponding oxygen-to-carbon ratio across the interface informed by EDX. i,j) XPS spectra near the C1s region and j) pore size distributions characterized by mercury porosimetry for cellulose (top) and LIG-E (bottom), \( n = 1 \). k) Cross-sectional photographs for the four different types of fabricated channels. From left to right: flow-through paper, flow-through LIG-E, lateral-flow paper, and lateral-flow LIG-E. The yellow dashed lines define channel boundaries confined with wax barriers. Scale bar: 500 \( \mu \)m.

Raman spectroscopic analysis of the pyrolyzed cellulose revealed further details on the formation of graphenic material (Figure 2c). For superficially pyrolyzed samples, the fluorescence signal from the cellulose paper dominates, but this disappears as the electrical resistance decreases. In addition, the peaks characterizing the sp²-hydrizidized carbon network (G band) and the finite lateral size of the graphitic crystallites (D band)\[38\] emerge at 1577 ± 2 and 1339 ± 2 cm\(^{-1}\), respectively. By increasing the laser power from 2.4 to 4.8 W, the ratio of D-band to G-band peak areas gradually decreases, indicating lateral growth of crystalline domains\[38\]. Conversely, the 2D band at 2665 ± 5 cm\(^{-1}\), originated from the D-band overtone and sensitive to graphene stacking\[39\] becomes more prominent as laser power increases, evidencing the emergence of thin graphene domains. The multi-component and broadband nature of the 2D-overtone (Figures S3 and S4, Supporting Information) further suggests a high degree of graphitization with turbostratic stacking between the graphenic layers\[36\]. Notably, we did not observe significant shifts in peak positions upon growth of the crystallite domains (Figure S5, Supporting Information).
Early reports on the formation of laser-pyrolyzed conductive materials have relied exclusively on Raman spectroscopy.\cite{40} However, this approach provides a qualitative, or at best semiquantitative, assessment of structural parameters. To gain quantitative insights into the evolution of their structural parameters, we carried out wide-angle X-ray scattering (WAXS) on the successfully graphenized samples to correlate materials conductivity with graphenic crystallography. After isolating the pyrolyzed material from the cellulose, we were able to identify diffractiongrams of graphitic materials exhibiting the (002), (10) , and (11) diffraction peaks (Figures 2d and Figure S6, Supporting Information). It should be noted that turbostratic layered materials have indistinguishable (101) and (100) peaks, and are thus assigned as (10) here; the same applies to the (11) peak.

We estimated the crystallite size of our pyrolyzed materials using the Scherrer equation.\cite{35,18} This analysis revealed that by increasing the laser power from 2.4 to 4.8 W, the crystallite lateral size, \(L_c\), extracted from the (10) peak, grows from 3.5 ± 0.4 to 4.6 ± 0.1 nm. On the other hand, the crystallite thickness \(L_t\), extracted from the (002) peak, reduces from 3.8 ± 0.4 to 1.32 ± 0.04 nm, corresponding to \(10 \pm 1\) and 3.6 ± 0.1 stacking layers of graphene, respectively (Figure 2e). Similar crystallite parameters could be attained in wood samples pyrolyzed in a furnace at between 1000 and 2000 °C.\cite{35} Furthermore, upon increasing the laser power, the average interlayer distance informed by the \(d\)-spacing of the (002) peak, \(d_{002}\), gradually decreases from 0.4 nm to 0.37 nm, approaching that for AB-stacking graphite (0.335 nm), in spite of its turbostratic nature. The graphenic crystallites appear to grow laterally and interconnect, resulting in 7-fold drop in macroscopic electrical resistance. Furthermore, the nanometer-scale crystallite sizes, combined with their reduced thickness (a few layers), offer edge-rich graphene for efficient electrochemical detection (Figure S7, Supporting Information).\cite{42}

It is worth mentioning that previous studies for laser-pyrolyzed graphenic materials estimated the crystallite sizes from the Raman D/G ratio using a popular model established by Cançado et al.\cite{18,30,38} Compared to our values informed by WAXS, we found that the Cançado model overestimates the lateral dimension by four times (Figure S8, Supporting Information). This is unsurprising as the semipirical model was developed for top-down fabricated, highly pure nanographite samples, rather than semicrystalline materials or materials derived from precursors containing heteroatoms. As an aside, whilst the community adopted the term “laser-induced graphene” to refer to this class of materials, we have opted to use “nanographite,” or more generally graphenic (nano)material, to be consistent with the recommended nomenclature.\cite{39}

In practice, the macroscopic structural and surface properties of the pyrolyzed paper heavily influence LIG-E wetting and electrochemical responses in functional devices. To explore these features, we studied LIG-E using electron microscopy, and discovered that the fibrous structure of cellulose is conserved after pyrolysis (Figure 2f,g). As anticipated, analysis of energy-dispersive X-ray (EDX) spectra revealed that pyrolysis successfully removed over 95% of the oxygen atoms from the bulk paper material (Figure 2h). Interestingly, we did not detect any significant incorporation of nitrogen or sulfur atoms in the carbonaceous structure (Figure S9, Supporting Information).

Advanced chemical analysis by the X-ray photoelectron spectroscopy (XPS) corroborated the EDX results. Despite a significant reduction of oxygen content, we still observed a considerable fraction of C–O and C=O surface functional groups (Figure 2i). These hydrophilic functional groups are desirable to retain good wettability and could serve as anchor points for surface functionalization. Mercury porosimetry further revealed that the cellulose paper and LIG-E exhibit nearly identical mean pore sizes (11 μm), with a small degree of distribution broadening (Figure 2j). The conservation of cellulose wetting and micrometer-scale porosity after laser pyrolysis makes LIG-E extremely promising for applications in capillary-driven electrofluidic systems.

To explore the seamless integration of LIG-E with fluidic channels, we combined laser-induced pyrolysis with double-layer lamination (top and bottom) of prepatterned wax. Depending on the configuration, capillary flow can either extend through the whole sheet (vertical channels) or confine within the electrode depth along the surface (lateral channels) (Figure 2k). Importantly, we found that the conductive properties remain unaffected by the wax channel interfaces (Figure S10, Supporting Information). Additionally, it is worth noting that the electrodes retained their conductive properties even when subjected to a bending radius as low as 6 mm, thus making them promising for wearable sensors (Figure S11, Supporting Information).

2.2. Engineering Anisotropic Capillary-Flow Properties

Next, we examined and engineered the wicking properties of our channel architectures in various flow configurations, since effective wetting within the porous LIG-E structure is essential to maximizing electrode utilization for sensing applications. The wetting properties of laser-pyrolyzed polyimide can be tuned by control of the lasing atmosphere.\cite{44} K\textsubscript{2}MnO\textsubscript{4} pretreatment,\cite{45} and post-modifications.\cite{46} In our cellulose systems, we found that the laser-pyrolyzed electrodes are always superhydrophilic, completely absorbing a water droplet within <50 ms. This is comparable to unmodified cellulose paper (Figure 3a) regardless of the lasing atmosphere (Figure S12, Supporting Information). It should be noted that we used “wetting time” to evaluate hydrophilicity since water contact angles cannot be measured on wicking substrates. Importantly, the LIG-E fabricated on paper remained superhydrophilic after more than a week of storage under ambient conditions (Figure S13, Supporting Information). On the other hand, we rendered paper or LIG-E hydrophobic (static water contact angles of 117 ± 8° and 129 ± 2°) through lamination of a wax pattern (Figure 3a). This technique opened up the possibility of creating flow channels that are unaffected by the presence of electrodes and isolate the electrode contacts from the fluidic channel (Figure S14, Supporting Information).

Although assessment of static wetting properties offers useful information, we questioned whether the results could be transferred to more intricate flow-based systems. Paper-based devices are generally designed around specific flow configurations, such as lateral flow (with the front moving in-plane along the paper sheet), vertical flow (with the flow perpendicular to the stacked layers), or a combination thereof (3D paper microfluidic networks). This is an important aspect to consider because each flow configurations offer specific benefits for biosensing
applications. However, other electrode fabrication approaches, such as screen-printing, have limited applicability in the vertical flow format due to low permeability for out-of-plane flow.\[47\] Our permeable LIG-E becomes particularly intriguing in this regard. The directional nature of the lasing process results in the formation of anisotropic structure in LIG-E, which might interact with fluid in unique manner depending on the flow direction. To explore this, we flowed water through LIG-E embedded in cellulose and compared the fluid front positions as a function of time for neat paper, LIG-E, and oxygen plasma-treated LIG-E. The shaded areas correspond to fits to the Washburn equation according to $L = (D_w \eta)^{0.5}$ where $L$ is the front position, $D_w$ is the Washburn diffusion coefficient and $t$ is time.\[50,51\] We found that the LIG-E diffusion coefficient in lateral flow reduces approximately by six-fold compared to untreated paper or plasma-treated LIG-E (Figure 3d).

Interestingly, while wicking through lateral channel networks has been extensively studied,\[32\] the vertical flow dynamics across multilayers structures in an out-of-plane direction have never been explored, despite their applications in many commercial diagnostic devices.\[33\] Surprisingly, we found that vertical flows exhibit Washburn diffusion coefficients approximately 5-fold lower than their lateral counterparts (Figure 3g), despite significantly shorter timescales and smaller diffusion distances. We hypothesize that the slower wicking observed in vertical configurations is due to the in-plane fiber direction and nonideal contact between cellulose layers.

2.3. Linking Capillary Wetting to Electrochemical Properties

In view of the anisotropic flow properties of the LIG-E, we examined its electrochemical characteristics with the aim of correlating these with capillary properties. The permeable electrodes and their unique wicking properties form the building block of the electrochemical platform. For this reason, understanding the effect of wetting on electrochemical performance is essential. We designed and fabricated our electrochemical sensors using a three-electrode configuration, in which voltages are applied and reported relative to a pseudoreference LIG-E, instead of a standard reference electrode, such as silver/silver chloride. This way, the simplicity and scalability of the fabrication process is greatly improved, while still being sufficiently accurate for almost all electrochemical sensing methodologies.

First, we investigated the effect of LIG-E wettability on the effective electroactive areas using a standard redox probe (ferro/ferricyanide) in two different flow configurations (Figure 4a). We interrogated the electrodes using cycling voltammetry (Figure 4b) and computed the electroactive area using the Randles–Ševčík equation for diffusion-controlled processes (Figure 4c).\[34\] The electrochemical porosity factor, $\eta$, is defined as the ratio of the electroactive area to the projected area (from the design). In lateral flow, we found that $\eta = 1 \pm 0.4$ for LIG-E due to poor wettability, but is drastically increased ($\eta = 4.0$) in oxygen plasma-treated LIG-E (Figure 4d). On the other hand, and echoing the moving front experiment, we observed high porosity factors in the vertical flow format for both LIG-E and plasma-treated LIG-E, showing $\eta = 5.7 \pm 0.2$ and $6.3 \pm 0.3$, respectively. These findings suggest that the top surface is both hydrophilic and electroactive, although it is not fully accessible in lateral flow configurations.
Figure 4. LIG-E electrochemical properties depend on electrode wicking. a) Electrochemical characterization of three-electrode cells made of LIG-E in lateral (top) and vertical (bottom) flow configurations. b) Comparison of cyclic voltammetry responses for LIG-E and plasma-treated LIG-E using $10 \times 10^{-5}$ M $[\text{Fe(CN)}_6]^{3-/4-}$ in 1 M KCl at scan rates of 12, 30, 50, and 80 mV s$^{-1}$. c) Randles–Ševčík plots derived from the current peak heights ($i_{\text{peak}}$) with respect to scan rate, together with linear fittings. d) Extracted electroactive areas and corresponding electrochemical porosity factors. e) Nyquist plots revealing electrochemical impedance for LIG-E and plasma-treated LIG-E in lateral or vertical flow configurations. Inset: the Randles circuit used to fit impedance responses (dotted lines) and extract the electron–transfer rates in (f). g) Statistical distribution ($n=18$) of extracted electroactive area values, revealing small device-to-device variations. h) Comparison of storage stability at room temperature and with desiccant over a period of four weeks for LIG-E and plasma-treated LIG-E.

We next evaluated the electron–transfer rates of the LIG-E using impedance spectroscopy (Figure 4e).\[^{[55]}\] In most cases, fast electron transfer rates are desirable as they usually lead to lower Ohmic overpotentials and sharper peaks during potential sweeps. We observed that the top layer of the LIG-E, which is accessible only in the vertical flow configuration, shows a higher electron rate constant (Figure 4f). Unexpectedly, oxygen plasma treatment also enhances the electron transfer rate. Our hypothesis is that partial etching of the LIG-E material or the presence of contaminants increases the number of exposed graphenic edges, which in turn facilitates interfacial reaction kinetics.\[^{[42]}\] Compared to other systems, the rate constant values reported here ($k_0 \approx 0.01$ cm s$^{-1}$) are approximately one order of magnitude higher than those fabricated by carbon screen printing and conventional laser pyrolyzation, but lower than the laser-pyrolyzed polyimide (Table S3, Supporting Information).\[^{[21,32,55]}\]

We further systematically characterized the electrochemical parameters of fabricated LIG-Es to evaluate the device-to-device variation and storage stability, which are important considerations for commercial applications and field deployability. Taking the electroactive area as the key index, our preliminary analysis indicated a device-to-device variation of less than 8% relative standard deviation (Figure 4g) and activity loss of below 30% over four weeks of storage at ambient temperature (Figure 4h).
Interestingly, oxygen plasma treatment improved storage stability, which we attribute to irreversible hydrophilization of the LIG-E surface,\textsuperscript{49} retaining electrode wetting characteristics that yield consistent signal magnitude upon storage.

With the above results in mind, we concluded that the porous conductive structure of LIG-E presented here successfully translates into stable and large electroactive surfaces for electrochemical detection, with fast electron transfer rates.

2.4. Lateral Flow Injection Analysis of Serum Samples

Flow injection analysis (FIA) is a high-throughput analysis method in which samples are injected sequentially into a flow of carrying buffer upstream of an electrochemical detector.\textsuperscript{30} FIA paper-based devices driven by capillary flow have been reported for the analysis of small molecules in buffer or urine samples, using electrodes contacted to the paper surface.\textsuperscript{16,57} In comparison, our LIG-E approach offers two main advantages. First, it simplifies the device architecture by integrating the fluidic channel and electrodes together, and second, thanks to its embedded nature, it analyses the entire cross-section of the fluid flowing through the channel, rather than just the top surface in contact with the fluid (Figure S18, Supporting Information).

For the FIA application, we designed the device in a lateral flow configuration, which allows spatial separation of individual components, including buffer inlet, injection port, and electrodes, along the flow direction. As a clinically relevant assay, we chose to analyze alkaline phosphatase (ALP) in serum. ALP is a first-line biomarker for the diagnosis and treatment of liver, bone, and parathyroid diseases.\textsuperscript{58} Typical concentrations of serum ALP in adults range between 30 and 120 U L\textsuperscript{-1} (activity unit; 1 U = 1 μmol p-nitrophenol per minute at 37 °C).\textsuperscript{59} A deviation from this range represents the starting point of clinical decision algorithms for a variety of diseases, including hypophosphatasia.\textsuperscript{60}

Figures 5a,b presents a schematic and photograph of our FIA device. A steady capillary flow is first established between the buffer reservoir and absorbent pad, laterally moving along the channel and across the embedded LIG-Es. The sample is mixed with the p-aminophenyl phosphate (p-APP) substrate, incubated, and then injected into the device upstream of the LIG-Es. We performed real-time detection via chronoamperometry (Figures 5c and Figure S19, Supporting Information). Our optimized protocol allows the injection and analysis of up to 24 samples within 20 min, consuming less than 500 μL of carrying buffer and 5 μL of each sample (Figure 5d). For the spiked buffer samples, the assay exhibits good linearity within the clinically relevant range, with a detection limit of 1.4 U L\textsuperscript{-1} (Figure 5e); a value comparable with the lower working range of gold-standard benchtop systems.\textsuperscript{61}

For the analysis of serum samples, we found that the effects of the complex sample matrix and increased viscosity hinder the comparison with predetermined calibration values. Accordingly, we used the standard addition method, which has been shown to effectively mitigate matrix contributions in calibration-free protocols.\textsuperscript{62} We analyzed three serum samples and found alkaline phosphatase activities of 35 ± 1, 105 ± 6, and 8 ± 4 U L\textsuperscript{-1} (Figure 5f,g). Remarkably, and despite the large surface area of LIG-E, we did not observe considerable electrode fouling in serum tests. We attribute this to the low-volume requirements and the regeneration of electrode surface by the buffer flow. We benchmarked against the gold standard test, a plate reader monitoring absorption kinetics with p-nitrophenyl phosphate as a substrate (Figures S20 and S21, Supporting Information), and observed excellent agreement (33.6 ± 0.6, 106.7 ± 0.5, and 7.4 ± 0.1 U L\textsuperscript{-1}, respectively; Figure 5h) between the datasets.

2.5. A Vertical Flow Capture Assay for the Detection of HPV16-Activated CRISPR Reporters

Capture assays, such as pregnancy and Covid-19 antigen tests, represent the most popular current application of μPADs. In these assays, capillary-driven flow is harnessed to minimize the number of user operations (most notably washing steps) compared to plate-based assays, making these devices particularly suitable for decentralized testing. Recently, the introduction of CRISPR-based biosensing has expanded our collective ability to perform molecular diagnostics at the point of care.\textsuperscript{63-65} An excellent example is the DNA Endonuclease-Targeted CRISPR Trans Reporter (DETECTR) assay, which combines recombinase polymerase amplification (RPA) with CRISPR/Cas12a signal generation to detect viral genomes with exceptional sensitivity and on short timescales.\textsuperscript{63} As the field expands, the need for methods that detect CRISPR reporters using minimal instrumentation is becoming more pressing.\textsuperscript{64,65} With this in mind, and as a proof of concept, we developed a rapid electrochemical capture assay for HPV16, a high-risk carcinogenic subtype of HPV that benefits from early detection.\textsuperscript{66} Our approach integrates the DETECTR assay with electrochemical detection of the CRISPR reporters within our low-cost platform. Due to the “signal-off” nature of reporter detection (i.e., a strong positive sample leads to a low signal), electrochemical readout is highly advantageous, as it simplifies result interpretation by providing an unambiguous digital result for the untrained user.

We chose to construct the device around a vertical flow configuration (Figure 6a,b). Although vertical flow assays are less common than their lateral flow counterpart, they have had considerable recent commercial success due to the faster assay time resulting from enlarged flow cross sections.\textsuperscript{31} The fully permeable nature of the LIG-E is crucial here. We notice that early attempts at vertical-flow electrochemical devices demand complicated design involving actuated rotating layers, in order to circumvent poor permeability of screen-printed electrodes.\textsuperscript{67} Taking advantage of the inherent flow-through characteristics of vertical flow devices, our design sandwiches a nitrocellulose capture layer between a receiving sample pad and the permeable LIG-E, eliminating the need for laborious chemical functionalization of electrode. The working principle relies on the capture of ss-DNA reporters on the antibody-functionalized nitrocellulose pad (Figure 6c). Specifically, in the presence of HPV16 amplicons, reporters are cleaved and labels flow through the LIG-E without generating signal. Conversely, for a negative sample, reporters remain uncleaved, thus ensuring ample binding sites for labelling. Labelling and signal generation then take place through amplification of ALP, a standard enzymatic label for linked immunoassays (Figure S22, Supporting Information).

We designed the device to saturate after the addition of enzymatic substrate and quantified the amount of captured
Figure 5. Lateral flow injection analysis of alkaline phosphatase in serum. a) Exploded-view schematic of the device architecture. A steady capillary flow is established between the buffer reservoir and absorbent pad, laterally moving along the channel and across the embedded LIG-Es in the electrofluidic layer. b) Photograph of the assembled device connected to a potentiostat. c) Schematic diagram of the ALP detection assay in serum, with real-time detection on the porous electrodes allowing injection of multiple samples in sequence. d) Measurement of ALP activity in spiked buffer samples in a dilution series. e) Corresponding signals from the integrated peaks with respect to the ALP activity. The shaded line represents the mean with three standard deviations of the negative control. f) Analysis of the ALP activity of three unknown serum samples by the standard addition method. g) The ALP activities were extracted by linear fittings of the response signals. h) Comparison of measured ALP activity values with those from the gold-standard colorimetric test. p-AP: p-aminophenol; QI: 4-quinoneimine.
3. Conclusions

We have presented a platform that combines paper microfluidics and laser-pyrolyzed electronics. We elucidated the formation of nanoscale graphenic domains upon laser-induced pyrolysis of cellulose and found that the LIG-E not only conserves the microscale structure and macroporous nature of cellulose fibers, but can also retain the wetting and wicking behavior due to the oxygen-rich surface functional groups. The process enables the independent design of capillary and electronic current pathways and overlays. The LIG-E exhibits high electrochemical porosity and electron transfer rates. We have demonstrated two clinically relevant assays using the lateral and vertical flow configurations. The former is a flow injection analysis device for alkaline phosphatase detection of serum samples, showing high throughput (>1 assay per minute) and accurate calibration-free quantification by standard addition. The latter is a capture assay for the detection of DETECTR reporters, reaching a low HPV16 detection limit of 1 copy μL⁻¹ with rapid electrochemical readout. We anticipate that the unique porous morphology together with the high conductivity and electroactivity of LIG-Es could open doors to new applications in the field of clinical diagnostics, environmental and food monitoring, wearable sensing, and the broader realms of material electronics.

4. Experimental Section

Fabrication of the Electrofluidic Layers: Cellulose paper (CF3, Cytiva) was saturated with 0.8 M (92 g L⁻¹) ammonium sulfamate (NH₄SO₃NH₂, > 98%, Sigma) using a brush and left to dry overnight. Next, the LIG-Es were fabricated using a CO₂ laser engraver (100 W, Speedy 300, Trotec) equipped with a 1.5 inch focus lens and operated using the following parameters (unless indicated otherwise): power 18 (measured value: 4.8 W), speed 5 (measured value: 16 cm s⁻¹), defocus 10 mm, laser pulsing 1000
pulses per inch (PPI), line spacing 333 lines per inch (LPI). The lasing process was performed under a constant stream of nitrogen. The LIG-Es were then rinsed with deionized water, isopropanol and acetone and left to dry overnight. Optionally, the LIG-Es were treated by oxygen plasma for 90 seconds at 90 W (Atto, Diener electronic). Wax patterns were created by first printing a full layer of wax (Xerox Colorqube 8570) on a transparency (X-100, Folex), following by removal of the hydrophilic channel areas using the laser cutter (power 6, speed 1). The wax pattern was transferred onto the paper layer via lamination at a temperature of 110 °C (Photronics 325isi, CMP). All designs (channels and electrodes) are created in Adobe Illustrator CS6.

Structural and Chemical Characterization: The sheet resistance, $R_s$, (unit: Ω sq$^{-1}$) was measured using the four-probe technique, with the probes configured in a square with 2 mm spacing. The sheet resistance was calculated according to:

$$R_s = \frac{2\pi}{\ln 2} \frac{E}{i_0} (1)$$

where $E$ (in V) and $i$ (in A) are the applied voltage and measured current, respectively.[67]

Raman spectroscopy was performed using a confocal Raman microscope (Renishaw InVia) using a 532 nm laser (max power 50 mW), a 20x objective (Zeiss) and a 1800 lines mm$^{-1}$ grating. The exposure time was set to 3 s for a laser power of 5%, and spectra were recorded between 1237 and 2796 cm$^{-1}$ and averaged over 10 accumulations. Spectra were corrected for background effects by subtracting a linear function that compensates for autofluorescence of the cellulose paper. Peaks were analyzed by fitting a Lorentzian function with four components for the D-, G-, 2D- (double, 2D, and 2D$_s$) bands respectively,[16,18] i.e.,

$$f = \sum_{i=1}^{4} \frac{a_i}{1 + \left(\frac{\lambda - \lambda_i}{\Gamma_i}\right)^2} (2)$$

The individual integrated peak signals $S_i$ are given by $S_i = \pi a_i \lambda_i$, and used for analysis and discussion.

Wide-angle X-ray scattering (WAXS) measurements were performed using a laboratory powder X-ray diffractometer (XPerX Pro, PANalytical). The X-ray tube was operated at 45 kV and 40 mA with Cu Kα radiation (0.1542 nm). The LIG-E material was scraped off the cellulose paper and gently placed on a zero-diffraction plate. Measurements were performed from 2θ = 8° to 2θ = 100° with a step size of 0.2°. The length of the scattering vector, $q$, (in nm$^{-1}$) is given by $q = 4\pi \sin(\theta)/(2\lambda)$, with $2\theta$ being the scattering angle and $\lambda$ the X-ray wavelength ($\lambda_{CuKα} = 0.1542$ nm). The three main peaks considered are the (002), (101) and (110) peaks. The shoulders observed on the (101) and (110) peaks are attributed to higher order planes, namely (004) and (006), respectively, and were not accounted for during the fitting process due to their minor contributions. Crystallite dimensions were calculated using the Scherrer equation, which considers the broadening of scattering peaks in reciprocal space.[44] Each peak was fitted individually using a Gaussian peak function on top of a linear background.[15] The crystallite dimensions were estimated using:[45]

$$L = \frac{Kq}{\omega} (3)$$

where $K$ is an application-specific coefficient and $w$ the full width at half maximum of the scattering peak. We used $K = 0.91$ for $L_{002}$ from the (002) peak and $K = 1.84$ for $L_{001}$ from the (100) peak as defined by Warren.[41] The Scherrer equation has been shown to be valid for graphic materials with crystallite sizes above 2 nm.[15] The interlayer spacing was computed from the (002) peak position using Bragg’s law in the reciprocal space, i.e., $d_{002} = 2\pi q/$.

Scanning electron microscopy (SEM) measurements were performed on a digital field emission SEM (Ultra 55, Zeiss) with an electron beam energy of 5 keV, an aperture of 30 μm, and secondary electron detector

$$L = 2.69 \times 10^5 n^{3/2} AD^{1/2} C^{1/2} (4)$$

where $n$ is the number of electrons transferred, $A$ the electroactive area (in cm$^2$), $D = 6.0 \times 10^{-3}$ cm$^2$ s$^{-1}$ the diffusion coefficient of ferro/ferricyanide (in cm$^2$ s$^{-1}$). C the redox probe concentration (in mol cm$^{-3}$) and $\nu$ the scan rate (in V s$^{-1}$). The electrochemical porosity factor ($n$) was calculated by dividing the electroactive area by the geometric (projected) area of the design. Electron transfer rates were measured by electrochemical impedance spectroscopy (EIS) on a potentiostat (Vicon, Metrohm) using the same redox probe solution as above, and with the following parameters: DC offset of 0 V vs open-circuit potential, 10 mV amplitude, frequency range from 1 Hz to 200 kHz.[55] A Randles circuit was fitted to the high-frequency data in the EIS Nyquist plot using the Nova 2.1 software (Metrohm Autolab). The Randles circuit comprised a solution resistance, $R_s$, by two components in parallel: a constant phase element for the double layer,
Flow Injection Analysis Assay: Holders were designed in FreeCAD and 3D printed on a stereolithography 3D printer (SL15, Prusa) with transparent resin (Clear Tough Resin, 3DM) using the manufacturer standard parameters. All shapes of paper and nitrocellulose were cut to size with the laser cutter. The design included a buffer reservoir with 1 mL capacity, which is connected to the electrofluidic layer through a 3.8 mm diameter buffer pad (CF6, Cytiva). After flowing through the electrodes, the buffer was absorbed by two absorbent pads with 450 μL capacity each (CF6, Cytiva). The assay was prepared as follows. The sample (10 μL) was mixed with 10 μL of standard. The standard comprised alkaline phosphatase (P7923, Sigma) with a precalibrated activity. Next, 2 μL of 100 × 10^{-3} M p-aminophenyl phosphate (pA97%, Aldiogen) in 1 M Tris-HCl pH 9.8 with 200 × 10^{-3} M MgCl2 were added to the mixture followed by incubation for 20 min at 37 °C. The samples were put on ice before injection (5 μL injection volume) into the device. The following sera were analyzed: calf serum (C8506, Sigma), human serum H4522 (Sigma) and goat serum C9023 (Sigma). All sera samples were centrifuged at 2 krcf for 10 min before use. The electrochemical measurements were performed in chronamperometry mode (PGSTAT 204, Metrohm) with an applied voltage of 0.25 V vs the reference electrode, and sampling resolution of 10 ms. The signals were computed by integrating the current peaks with subtraction of a linear background.

For comparison, the alkaline phosphatase activities were evaluated on a plate reader using the standard colorimetric assay.[61] In short, 100 μL of sample was prepared containing the reference standard or serum at five-fold dilution in 100 × 10^{-3} M Tris-HCl pH 9.8 and 20 × 10^{-3} M MgCl2. Then 10 μL of 100 × 10^{-3} M p-nitrophenyl phosphate (p99%, Roth AG) was spiked into the sample in a 96-well plate and incubated at 37 °C. Absorption was monitored at 405 nm and the activity (in IU, defined as p-nitrophenol per min) calculated via the kinetics method using a two-sample Kolmogorov-Smirnov test. In the case of fitted curves, the confidence interval is shown as a shaded area for one standard deviation in each direction. The raw data is represented unless explicitly stated otherwise.

Supporting Information
Supporting Information is available from the Wiley Online Library or from the author.

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Conflict of Interest
Data Availability Statement

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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